

METHOD OF WINDING OPTICAL FIBER ON REEL

FIELD

The present invention relates to a method of winding
5 an optical fiber on a reel suitable for storage and
transportation of the optical fiber.

BACKGROUND

Conventionally, a technique has been keenly studied
10 to increase transmission capacity in optical transmission
using an optical fiber.

To increase transmission capacity in optical
transmission, an optical fiber for optical transmission is
required to be single-mode with the wavelength of use.
15 This is because, when transmission through an optical
fiber is performed in a plurality of modes, a mode
dispersion inevitably occurs due to a difference in group
velocity for each transmission mode, resulting in a
deterioration of signal waveform.

20 In view of this, a single mode optical fiber (SMF)
having a zero dispersion wavelength around the wavelength
of 1300 nm was used. By this optical fiber, an optical
transmission with transmission distance exceeding 100 km
and transmission capacity of several hundreds of Mbps were
25 realized. As shown, for example, in Fig. 6, this SMF had

a refractive index distribution structure composed of a central region 61 serving as the core and a clad 62.

On the other hand, since the transmission loss of an optical fiber becomes minimum around the wavelength of 1550 nm, it was desirable to perform optical transmission using this wavelength band. Therefore, a dispersion-shifted optical fiber (DSF) having a dual shape refractive index distribution structure and the zero dispersion wavelength around the wavelength of 1550 nm was realized.

Further, in these days, wavelength division multiplexing optical transmission system (WDM system) is being very actively studied and developed as a technique for further increasing transmission capacity. Then, an optical fiber suitable for use in WDM optical transmission is being examined from various viewpoints.

When using an optical fiber in WDM system, it is required that there should be no zero dispersion wavelength in the operating wavelength band, from the view point of preventing four-wave mixing. Thus, a non-zero dispersion-shifted optical fiber (NZDSF) has been developed. The NZDSF little involves four-wave mixing, so that, at present, it is regarded as most suitable for WDM system, and it is being rapidly put into practical use.

Further, taking into account broadband WDM system, some NZDSFs have a large effective core sectional area

(A_{eff}) in order to reduce non-linearity, and others have a reduced dispersion slope in order to decrease dispersion difference between wavelengths.

Specifically, the characteristics of a conventional DSF are, for example, as follows: A_{eff} , $50 \mu\text{m}^2$; dispersion slope, $0.07 \text{ ps/nm}^2/\text{km}$.

In contrast, an example of an NZDSF with an increased A_{eff} has the following characteristics: A_{eff} , $72 \mu\text{m}^2$; dispersion slope, $0.11 \text{ ps/nm}^2/\text{km}$. In this example, the emphasis is on the enlargement of A_{eff} .

An example of an NZDSF with a reduced dispersion slope has the following characteristics: A_{eff} , $55 \mu\text{m}^2$; dispersion slope, $0.045 \text{ ps/nm}^2/\text{km}$. In this example, the dispersion slope is reduced while maintaining an A_{eff} equal to or not smaller than that of the conventional DSF.

Some NZDSFs have characteristics other than those mentioned above. To achieve these characteristics, the refractive index distribution structure of NZDSFs tends to become more complicated than that of the conventional DSF.

Generally speaking, an optical fiber is shipped in a state, in which it is wound on a reel. A too-high winding tension when winding the optical fiber on the reel leads to an increase in transmission loss, whereas a too-low winding tension leads to loosen the winding on the reel due to vibration during transportation, and the like.

In particular, in the case of an NZDSF, the refractive index distribution structure is rather complicated as compared with that of a conventional DSF, in order to enlarge the A_{eff} and reduce the dispersion slope. Thus, the NZDSF is rather sensitive against bending and lateral pressure as compared with the conventional DSF.

For example, when wound at a bending diameter of 20 mm, the loss increase at a wavelength of 1550 nm is less than 1 dB/m in the conventional DSF, whereas it is approximately 5 dB/m in the optical fiber with reduced dispersion slope and approximately 20 dB/m in the optical fiber with enlarged A_{eff} .

Thus, it is important to optimize the winding condition of the optical fiber on a reel. For example, there is a method proposed as a method of winding a conventional DSF around a bobbin. In this method, the optimization of the winding condition is attempted by controlling the winding tension (0.1 N to 1 N) and the hardness of the barrel of the bobbin, in order to minimize an increase in transmission loss.

However, as stated in the above, the NZDSF is rather sensitive against bending and lateral pressure as compared with the conventional DSF. Thus, if the technique for a DSF is applied to the winding condition for the NZDSF, it

would lead to an increase in transmission loss.

Further, to minimize the increase in transmission loss due to lateral pressure in an optical fiber, it is necessary to take into account not only the tension but
5 also the winding diameter, winding pitch, and the like. Also from this viewpoint, the technique for winding DSF is to be regarded as incomplete.

Regarding DSFs including NZDSFs, it is known that minimizing the increase in bending loss is possible by
10 shifting the cutoff wavelength to the longer wavelength side in order to enlarge the A_{eff} .

However, while the conventional technique proves convenient for an optical fiber used around 1550 nm wavelength, it does not allow single-mode transmission
15 around the wavelength of 1300 nm, which means it is not suitable for optical transmission around the wavelength of 1300 nm.

Thus, at present, it is considered that an increase in bending loss is inevitable in an optical fiber suitable
20 for use in WDM system and intended for single mode operation around the wavelength of 1300 nm. There is a great demand for a technique for winding such an optical fiber on a reel, without increasing transmission loss and loosening the winding.

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SUMMARY

The present invention is a method of winding an optical fiber on a reel, utilizing

the optical fiber having the following characteristics:

- 5 • effective area A_{eff} is larger than $50 \mu\text{m}^2$,
- zero dispersion wavelength is outside a wavelength range of 1530 to 1565 nm,
- absolute value of the dispersion value in the entire wavelength range of 1530 to 1565 nm is in a range of 2
- 10 to 14 ps/nm/km, and
- bending loss at a wavelength of 1550 nm is in a range of 1 to 100 dB/m when wound at a diameter of 20mm; and
- the reel with a barrel diameter of not less than 100 mm and not more than 200 mm;

15 characterized by

winding the optical fiber on the reel with satisfying conditions of $d < p < 2d$ and $0.004 \leq (2T/D) \leq 0.007$, wherein d is a coating outer diameter of the optical fiber (mm), D is a barrel diameter of the reel (mm), T is a

20 winding tension (N), and p is a winding pitch (mm).

In this specification, the terms are based on the definitions according to ITU-T G. 650 unless defined specifically.

Other and further features and advantages of the

25 invention will appear more fully from the following

description, with referring to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a sectional view of a reel for
5 illustrating a winding method of an optical fiber on a
reel according to an embodiment of the present invention.

Fig. 2 is a diagram showing a refractive index
distribution structure of an optical fiber that is used in
a working example of a winding method of an optical fiber
10 on a reel according to the present invention.

Fig. 3 is a diagram showing another refractive index
distribution structure of an optical fiber that is used in
a working example of a winding method of an optical fiber
on a reel according to the present invention.

15 Fig. 4 is a diagram showing another refractive index
distribution structure of an optical fiber that can be
used in a winding method of an optical fiber on a reel
according to the present invention.

Fig. 5 is a diagram showing still another refractive
20 index distribution structure of an optical fiber that can
be used in a winding method of an optical fiber on a reel
according to the present invention.

Fig. 6 is an explanatory diagram showing the
refractive index distribution structure of an SMF.

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DETAILED DESCRIPTION

According to the present invention, there is provided the following means:

- (1) A method of winding an optical fiber on a reel,
5 utilizing
the optical fiber having the following characteristics:
- effective area A_{eff} is larger than $50 \mu\text{m}^2$,
 - zero dispersion wavelength is outside a wavelength range of 1530 to 1565 nm,
 - 10 • absolute value of the dispersion value in the entire wavelength range of 1530 to 1565 nm is in a range of 2 to 14 ps/nm/km, and
 - bending loss at a wavelength of 1550 nm is in a range of 1 to 100 dB/m when wound at a diameter of 20mm; and
- 15 the reel with a barrel diameter of not less than 100 mm and not more than 200 mm;

characterized by
winding the optical fiber on the reel with satisfying conditions of $d < p < 2d$ and $0.004 \leq (2T/D) \leq 0.007$,
20 wherein d is a coating outer diameter of the optical fiber (mm), D is a barrel diameter of the reel (mm), T is a winding tension (N), and p is a winding pitch (mm).

- (2) The method according to the above (1), wherein a cutoff wavelength of the optical fiber after formed as a
25 cable is not more than 1260 nm.

(3) The method according to the above (1), wherein the optical fiber has two or more annular regions between a central region and a clad, and the minimum refractive index of at least one annular region is negative.

5 The method of winding an optical fiber on a reel according to the above item (1) is accomplished as a result of intensive studies based on the experimentally ascertained fact that the winding conditions for the above optical fiber, which is sensitive against bending and
10 lateral pressure, are influenced more by the reel barrel diameter and the optical fiber winding pitch than by the hardness of the reel barrel portion.

 Further, by the method of the above item (1), it is possible to wind the optical fiber on a reel in a manner
15 suitable for storage, and transportation, such that no loosening of the winding occurs due to vibration during transportation, and the like, without increasing the transmission loss. As a result, it is possible to prevent breakage when letting out the optical fiber from the reel
20 to form it into a cable.

 It is desirable that a reel, around which an optical fiber is wound, is being as compact as possible and allows winding of a lot of optical fiber, from the viewpoint of reductions of storage cost and transportation cost. From
25 this point of view, it is desirable for the reel barrel

diameter D to be not more than 200 mm.

In some cases, the optical fiber is stored for a long period of time in a state, in which it is wound around the reel. Therefore, when the reel barrel diameter D is small, the optical fiber may result in breaking due to excess fiber strain. Thus, taking into account the reliability in long-term storage, it is desirable for the reel barrel diameter D to be not less than 100 mm. The reel barrel diameter is preferably in the range of 140 mm to 180 mm.

According to the method of winding an optical fiber around a reel according to the above item (2), an optical fiber, whose cutoff wavelength after formed into a cable is not more than 1260 nm, can be wound on a reel.

According to the method of winding an optical fiber around a reel according to the above item (3), even an optical fiber, which has two or more annular regions between a central region and a clad and in which fiber the minimum refractive index of at least one annular region being negative, can be wound on a reel without increasing the transmission loss and loosening the winding.

Embodiments of the present invention will now be explained with reference to the drawings.

Fig. 1 is a sectional view of a reel for illustrating a winding method of an optical fiber on a

reel according to an embodiment of the present invention. In Fig. 1, numeral 1 indicates a reel, and numeral 2 indicates an optical fiber. In Fig. 1, the first layer of the optical fiber 2 has been wound halfway.

5 The barrel diameter D of the reel 1 is not less than 100 mm and not more than 200 mm. The optical fiber 2, whose outer diameter after coated is d (mm), is wound on the reel 1 with a tension T (N) and at a winding pitch of p (mm). As shown in Fig. 1, the winding pitch p means the
10 distance between the centers of adjacent portions of the optical fiber 2 in the same layer.

 The optical fiber 2 is an NZDSF whose effective core sectional area A_{eff} is generally larger than $50 \mu\text{m}^2$, and preferably larger than $60 \mu\text{m}^2$. The optical fiber 2 has a
15 zero dispersion wavelength outside a wavelength range of 1530 to 1565 nm, and the absolute value of the dispersion value in the entire wavelength range of 1530 to 1565 nm is generally in a range of 2 to 14 ps/nm/km, and preferably in a range of 6 to 10 ps/nm/km. Further, the optical
20 fiber has a bending loss at a wavelength of 1550 nm, generally in a range of 1 to 100 dB/m, and preferably in a range of 1 to 50 dB/m, when it is wound at a diameter of 20 mm.

 The optical fiber preferably has a small dispersion
25 slope, and the dispersion slope is generally 0.10

ps/nm²/km or less, preferably 0.04 to 0.10 ps/nm²/km.

The transmission loss of the optical fiber is generally 0.25 dB/km or less, and preferably 0.19 to 0.22 dB/km. The increase in transmission loss before and after
5 wound on a reel is preferably 0.03 dB/m or less.

The coating outer diameter of the optical fiber is generally 0.23 to 0.27 mm.

When the optical fiber 2 is wound on the reel 1, the winding conditions are controlled so as to satisfy the
10 following conditions $d < p < 2d$ and $0.004 \leq (2T/D) \leq 0.007$, where D is the barrel diameter (mm) of the reel 1, T is the winding tension (N), d is the outer diameter (mm) of the optical fiber 2 after coating, and p is the winding pitch (mm). As a result, even the optical fiber 2, which
15 has the above characteristics and is sensitive against bending and lateral pressure, can be wound on the reel 1 without increasing the transmission loss and loosening the winding. It is further preferable to set the winding pitch to $1.5d < p < 2.0d$. In addition to this, it is
20 further preferable to set the winding tension to $0.005 \leq (2T/D) \leq 0.007$.

In accordance with the present invention, it is possible to wind an optical fiber without increasing the transmission loss. At the same time, the thus-wound fiber
25 is suitable for storage, transportation, and the like, and

is prevented from loosening due to vibration during transportation, and the like. As a result, the present invention is advantageous since it is possible to prevent breakage of an optical fiber when letting out the optical
5 fiber from the reel to form it into a cable. The method of the present invention is especially effective for winding a non-zero dispersion-shifted optical fiber.

The present invention will be described in more detail based on examples given below, but the present
10 invention is not meant to be limited by these examples.

EXAMPLES

Table 1 shows the characteristics of two optical fibers α and β of NZDSFs. Each of the optical fibers α
15 and β has a clad with an outer diameter of 125 μm , which is covered with two layers of an ultraviolet curing urethane acrylate type resin to exhibit a coating outer diameter of nominal 250 μm . In Table 1, the unit of dispersion is ps/nm/km, the unit of dispersion slope is
20 ps/nm²/km, and the unit of transmission loss is dB/km, and the unit of bending loss at a bending diameter of 20 mm is dB/m.

Table 1

| Name | Dispersion | Dispersion slope | Transmission loss | Bending loss | Structure |
|----------|------------|------------------|-------------------|--------------|-----------|
| α | 4 | 0.045 | 0.21 | 5 | Fig. 2 |
| β | 6 | 0.11 | 0.21 | 20 | Fig. 3 |

The optical fiber α has the refractive index distribution structure as shown in Fig. 2. The refractive index distribution structure has a first annular region 22 and a second annular region 23 between a central region 21 constituting the core and a clad 24. The refractive index of the central region 21 and the refractive index of the second annular region 23 are higher than the refractive index of the clad 24, and the refractive index of the first annular region 22 is lower than the refractive index of the clad 24. While the refractive index of the first annular region 22 in Fig. 2 is lower than the refractive index of the clad 24, it is also possible for the refractive index of the first annular region 22 to be approximately the same as the refractive index of the clad 24.

The optical fiber β has the refractive index distribution structure as shown in Fig. 3. The refractive index distribution structure has a first annular region 32, a second annular region 33, and a third annular region 34

between a central region 31 and a clad 35. Then, the refractive index of the central region 31 and the refractive index of the second annular region 33 are higher than the refractive index of the clad 35, and the refractive index of the first annular region 32 and the refractive index of the third annular region 34 are lower than the refractive index of the clad 35. While the refractive index of the first annular region 32 in Fig. 3 is lower than the refractive index of the clad 35, it is also possible for the refractive index of the first annular region 32 to be approximately the same as the refractive index of the clad 35.

The above optical fibers α and β were wound on reels having a barrel diameter D of 100 to 200 mm by a length of approximately 25 km. It was found out that when conditions $d < p < 2d$ (i.e., $0.25 < p < 0.50$) and $0.004 \leq (2T/D) \leq 0.007$ were satisfied, neither an increase in transmission loss nor loosening of the winding occurred, whereas when the condition $d < p < 2d$ or $0.004 \leq (2T/D) \leq 0.007$ was not satisfied, an increase in transmission loss or loosening of the winding occurred.

More specifically, when $p \geq 2d$, winding the optical fibers α and β could result that an optical fiber portion in an upper layer locally sunk between optical fiber pitches in a lower layer, thereby causing an increase in

transmission loss. When $(2T/D) < 0.004$, the winding tension T was deficient, so that there was a higher possibility of the loosening of the winding occurring. When $(2T/D) > 0.007$, the winding tension T was too large, and due to the influence of the lateral pressure applied to the optical fiber 2, the transmission loss increased. In particular, when $(2T/D) > 0.007$ and $p \geq 2d$, the increase in transmission loss could exceed the transmission loss of the optical fiber itself.

Table 2 shows the results obtained by winding optical fibers α and β on reels as described above. Regarding transmission loss, it was rated as "○" (good) when the increase in transmission loss was not more than 0.03 dB/km. Regarding winding, each reel was dropped in the direction of the central axis thereof from a height of 75 cm, and was visually checked for any such unwinding as would affect the subsequent winding. It was rated as "○" (good) when no such loosening was caused.

Table 2

| Fiber name | Reel barrel diameter D | Diameter after coated d | Winding pitch p | 2T/D | Transmission loss | Winding state |
|------------|------------------------|-------------------------|-----------------|--------|-------------------|---------------|
| α | 150 | 0.25 | 0.40 | 0.0035 | ○ | × |
| α | 150 | 0.25 | 0.40 | 0.0055 | ○ | ○ |
| α | 150 | 0.25 | 0.40 | 0.0075 | × | ○ |
| α | 150 | 0.25 | 0.45 | 0.0055 | ○ | ○ |
| α | 150 | 0.25 | 0.55 | 0.0055 | ○ | × |
| α | 170 | 0.25 | 0.40 | 0.0035 | × | ○ |
| α | 170 | 0.25 | 0.40 | 0.0055 | ○ | ○ |
| α | 170 | 0.25 | 0.40 | 0.0075 | × | ○ |
| α | 170 | 0.25 | 0.45 | 0.0055 | ○ | ○ |
| β | 150 | 0.25 | 0.40 | 0.0035 | ○ | × |
| β | 150 | 0.25 | 0.40 | 0.0055 | ○ | ○ |
| β | 150 | 0.25 | 0.40 | 0.0075 | × | ○ |
| β | 150 | 0.25 | 0.45 | 0.0055 | ○ | ○ |
| β | 150 | 0.25 | 0.55 | 0.0055 | ○ | × |
| β | 170 | 0.25 | 0.40 | 0.0035 | ○ | × |
| β | 170 | 0.25 | 0.40 | 0.0055 | ○ | ○ |
| β | 170 | 0.25 | 0.40 | 0.0075 | × | ○ |
| β | 170 | 0.25 | 0.45 | 0.0055 | ○ | ○ |

As shown in Table 2, even in the case of the optical fibers α and β whose refractive index distribution structures were rather complicated (as compared with a DSF) as shown in Figs. 2 and 3 and which were sensitive against bending and lateral pressure, the method of the present invention made it possible to wind them on reels

so as not to increase the transmission loss or loosen the winding.

In Table 2, when the value $2T/D$ was 0.0075, the condition corresponded to a condition for winding the conventional DSF on a reel. It is apparent that such the
5 condition was not appropriate as the conditions for winding the optical fibers α and β on reels. Thus, in the winding condition of the present invention, the value of $2T/D$ is smaller than that in the conventional winding
10 condition.

It goes without saying that the measurement results of Table 2 are only given by way of example and that the scope of the present invention is not restricted to this table.

15 If also goes without saying that the refractive index distribution structure of the optical fiber for the method for winding an optical fiber on a reel according to the present invention is not restricted to those shown in Figs. 2 and 3.

20 For example, it is also possible to adopt the refractive index distribution structure as shown in Fig. 4, which has a first annular region 42 and a second annular region 43 between a central region 41 and a clad 44. Further, the refractive index of the central region 41 and
25 the refractive index of the second annular region 43 are

lower than the refractive index of the clad 44, and the refractive index of the first annular region 42 is higher than the refractive index of the clad 44. While the refractive index of the second annular region 43 is lower
5 than the refractive index of the clad 44 in Fig. 4, this should not be construed restrictively. It is also possible for the maximum refractive index of the second annular region 43 to be higher than the refractive index of the clad 44.

10 Further, it is also possible to adopt the refractive index distribution structure as shown in Fig. 5, which has a central region 51, an annular region 52, and a clad 53. The refractive index of the central region 51 is lower than the refractive index of the clad 53, and the
15 refractive index of the annular region 52 is higher than the refractive index of the clad 53.

In the examples of the refractive index distribution structure of the optical fiber to be used in the method for winding an optical fiber on a reel of the present
20 invention, it is desirable at least one annular region has the minimum refractive index that is negative. However, this should not be construed restrictively, and a refractive index is freely selectable as long as it is not departing from the scope of the present invention.

25 Further, it is desirable for the optical fiber for

use in the method for winding an optical fiber on a reel
of the present invention to exhibit a cutoff wavelength of
not more than 1260 nm after it is formed into a cable,
whereby the optical fiber can be suitably used in WDM
5 system and it becomes possible to conduct single mode
operation around the wavelength of 1300 nm.

Having described our invention as related to the
present embodiments, it is our intention that the
10 invention not be limited by any of the details of the
description, unless otherwise specified, but rather be
construed broadly within its spirit and scope as set out
in the accompanying claims.